TANK REMOTE REPAIR SYSTEM CONCEPTUAL DESIGN (U)

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September 24, 2002

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This document was prepared in conjunction with work accomplished under Contract No. DE-AC09-96SR18500 with the U. S. Department of Energy.

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WSRC-TR-2002-00412

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EXECUTIVE SUMMARY

This document describes two conceptual designs for a Tank Remote Repair System (TRRS) to perform leak site repairs of double shell waste tank walls (Types I, II, III, and IIIA) from the annulus space. The first concept uses a magnetic wall crawler and an epoxy patch system and the second concept uses a magnetic wall crawler and a magnetic patch system. The recommended concept uses the magnetic patch system, since it is simpler to deliver, easier to apply, and has a higher probability of stopping an active leak.

BACKGROUND

The Savannah River Site (SRS) and Hanford have tanks and transfer systems that have exceeded their original design life, but may be used for waste processing for another 30-40 years. At SRS, the wastes from recovery of plutonium and uranium are stored in large, near-surface carbon steel tanks with multiple containment barriers to prevent leakage into the surrounding environment. The oldest tanks (ca. 1955) were constructed of carbon steel and most tanks are Double Shell Tanks (DST Type I,II,III) with an annulus space between the primary carbon steel tank wall and a concrete outer shell. In the past, leak sites have been detected in the primary vessel walls in some of the Type I and Type II tanks. At the present time there are no plans to build new tanks, therefore a process to repair leaks may be useful during waste removal from the tanks. However, due to various obstructions in the annulus space of the tanks there is no assurance that all leaks can be repaired. The repair task is further complicated by the limited size (5" diameter) and number of access risers on some SRS tanks.

The waste tank repair program is co-funded by the department of Energy (DOE) Office of Science and Technology (OST) and SRS HLW division. The OST will fund and manage the waste tank repair program with the Tanks Focus Area's (TFA) Task Technical Plan (TTP) SR18WT21 and TTP SR10C131. The Savannah River Technology Center (SRTC) Materials Technology Section (MTS) is responsible for developing a tank Leak Mitigation System (LMS) under TTP SR18WT21 and the SRTC Engineered Equipment & Systems (EES) department is responsible for integrating a delivery vehicle and the LMS under TTP SR10C131.

The TRRS Program Plan¹ outlines the entire program from development to deployment. The TRRS Development & Acquisition Strategy² outlines funding and general scope for each fiscal year. The LMS and Vehicle Functions and Requirements³.⁴ include the detailed functions and requirements for each system. The LMS Material Selection Program Plan⁵ outlines the LMS Evaluation work to be preformed. The LMS evaluation tests are in progress, and the LMS recommendation will follow soon. The TRRS strategy is shown in Figure 1, and this report is the first stage to the TRRS design and is an FY02 deliverable. Currently the task is not funded beyond FY02.

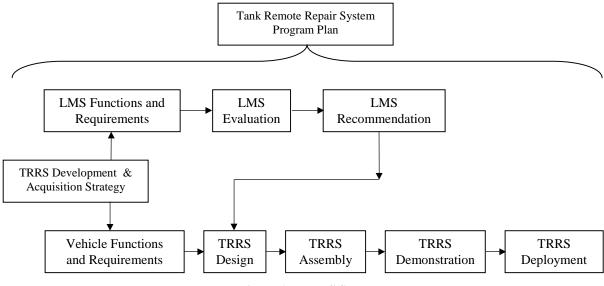


Figure 1 – TRRS Strategy

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ASSUMPTIONS

The following assumptions are made to complete the TRRS conceptual design report.

- SRS currently uses magnetic wall crawlers in the waste tank annulus space for visual and ultrasonic tank wall inspections. Due to the success of these magnetic wall crawlers, a similar crawler will be used as the TRRS vehicle. SRS is currently using the Force Institute AMS-1TM wall crawler.
- The leak sites needing repair are accessible via the annulus space between the primary waste tank and the secondary containment.
- The annulus space is accessible via 5.0 inch (or greater) inner diameter risers.
- The TRRS will only repair leaks on the exterior primary tank wall, not the knuckle or tank bottom.
- The TRRS will traverse weld beads and other wall imperfections (i.e. weld and concrete splatter) that are not greater than 0.5 inches high.
- Obstructions in the tank annulus (ventilation ducts, pipes, etc.) may make some tank wall areas inaccessible to the TRRS.

CONCEPTUAL DESIGNS

Figure 2 shows the overall concept for the TRRS. The vehicle, cameras, lights, and patch system will be controlled by a mobile cabinet located on the tank top. A long tether will connect the vehicle to the control cabinet. The vehicle will be deployed in the annulus space between the primary tank wall and the secondary containment on the primary tank wall exterior. The appendix includes details about Type I, II, III, IIIA tanks. This is the basic configuration currently used in SRS tank wall inspections, and has a proven record of success.

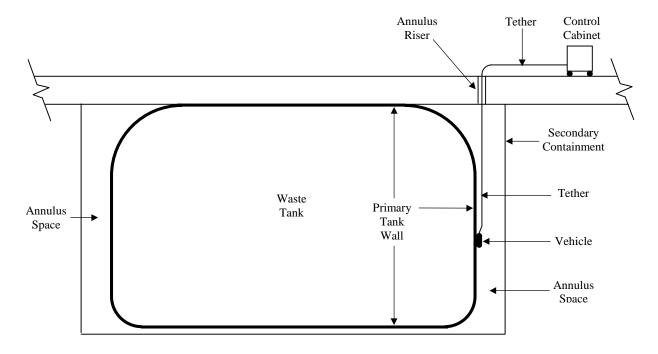


Figure 2 – TRRS Concept

Figure 3 shows a typical magnetic wall crawler, the Force Institute AMS-1TM, the pneumatic control unit, PCU-7 and the power supply, MDU-13. The TRRS concept is based on this magnetic wall crawler due to the past successful use at SRS for tank annulus visual and UT inspections.

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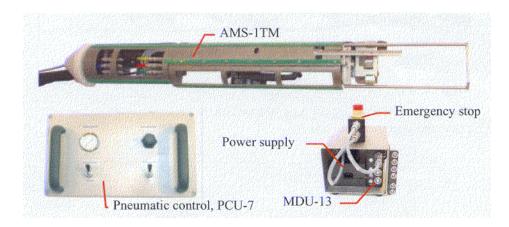


Figure 3 - Force Institute AMS-1TM Wall Crawler

The LMS evaluation work looked at several tank repair options and determined two feasible concepts. The first concept is an epoxy based patch and the second is magnetic based patch. The following sections describe these concepts, how they would be integrated with a magnetic wall crawler to make the TRRS, and the advantages and disadvantages for each.

Epoxy Patch Concept

The LMS evaluation includes testing several epoxies under various conditions, but the delivery and application details are similar for all epoxies. The two epoxy parts need to be mixed shortly before the epoxy is applied to the tank wall. The individual parts must be relatively thick so the mixed compound will adhere to the vertical tank wall during the epoxy curing time. The crawler will carry the epoxy parts to the leak site, mix the parts, and apply the epoxy to the tank wall over the crack and surrounding area. The applicator/mixer will be similar to the "double syringe" dispenser used by some commercial epoxies. The two epoxy parts are stored in separate syringe tubes that share plunger handles and outlet tip. The mixing occurs in the outlet tip. The epoxy will form a water-tight seal around the crack. Figure 4 shows a conceptual epoxy patch cross section.

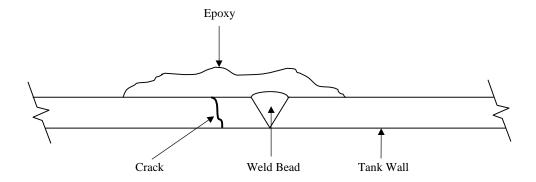


Figure 4 – Epoxy Patch Cross Section

After testing several epoxies, MTS determined that pumping the mixed, or unmixed, epoxy through long small diameter tubing is impractical due to the materials high viscosity. The only practical solution is to carry the two epoxy parts on-board the wall crawler and mix them at the leak site. Figure 5 shows the epoxy "double syringe" dispenser concept.

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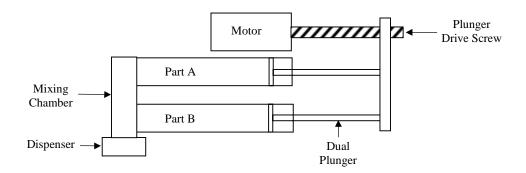


Figure 5 – Epoxy Dispenser Concept

Figure 6 shows the Force Institute magnetic wall crawler with an epoxy dispenser. The crawler is 41.73 inches long, 4.75 inches in diameter, and is drawn to scale. The epoxy dispenser is located in the area usually used for ultrasonic sensors. The epoxy dispenser was designed to fit in this existing space, so the commercial crawler would not require significant changes.

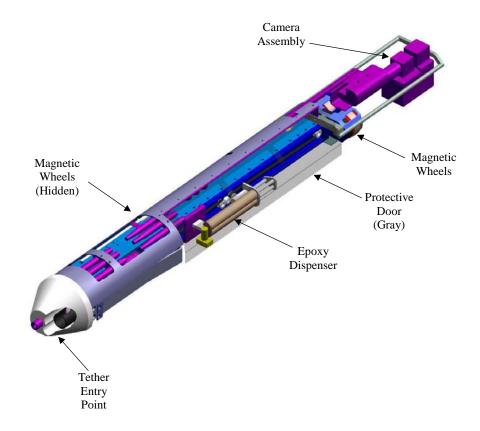


Figure 6 – Wall Crawler with an Epoxy Applicator

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Figure 7 shows a close-up bottom view of the epoxy dispenser. The epoxy dispenser can be moved back and forth in the crawler cargo area with the device that normally moves the ultrasonic sensors. If a larger quantity of epoxy is required, this functionality could be removed and larger epoxy tubes could be used.

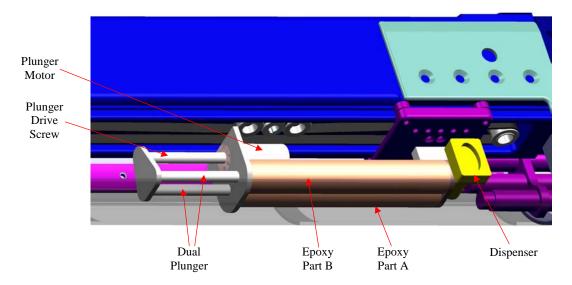


Figure 7 - Epoxy Dispenser, Bottom View

The following are advantages to the epoxy concept are:

- Testing showed the epoxies should work under the assumed conditions.
- Future tank wall analysis (UT testing) can be done through the epoxy material.

The following are disadvantages to the epoxy concept:

- Remotely mixing and dispensing epoxy in the tank annulus is untested and risky.
- Applying epoxy in the tank annulus is untested and risky.
- The limited supply of epoxy onboard limits the number of cracks that can be sealed per deployment.
- Examining the tank wall through the epoxy material is untested.
- There is a low probability the system will work on active leak sites.

Magnetic Patch Concept

The LMS evaluation includes testing a novel magnetic patch concept. The crawler will carry the magnetic patch with small deployment arm. The vehicle will maneuver the patch above the leak site and the arm will be actuated to place the patch over the crack. The patch rare earth magnets pull the backing plate towards the tank wall. The backing plate compresses the seal material against the crack and surrounding tank wall. The seal material will form a water-tight seal around the crack. Figure 8 shows the magnetic patch concept cross section.

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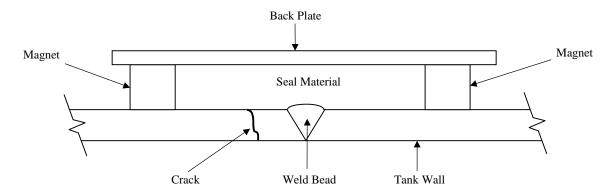


Figure 8 – Magnetic Patch Cross Section

Figure 9 shows the Force Institute magnetic wall crawler with the magnetic patch. The crawler is 41.73 inches long, 4.75 inches in diameter, and is drawn to scale. The magnetic patch is located in the area usually used for ultrasonic sensors. The magnetic patch and deployment arm were designed to fit in this existing space, so the commercial crawler would not require significant changes.

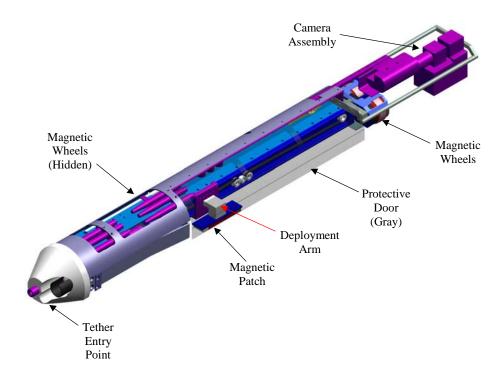


Figure 9 - Wall Crawler with Magnetic Patch

Figure 10 shows a close-up bottom view of the magnetic patch. The deployment arm, which holds the patch, can be moved back and forth in the crawler cargo area with the device that normally moves the ultrasonic sensors. The magnetic patch shown is 1 inch by 4 inches. If a larger magnetic patch is required, this functionality could be removed and a larger patch could be used.

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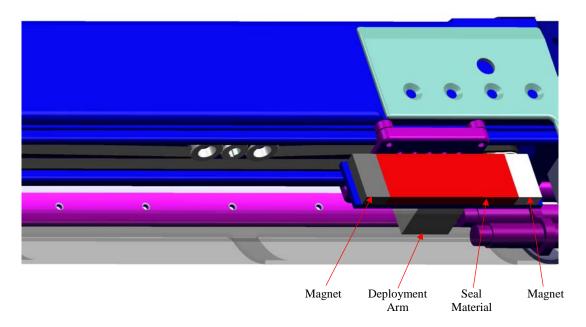


Figure 10 - Magnetic Patch, Bottom View

The following are advantages to the magnetic patch concept:

- Testing showed that the magnetic patches should work under the assumed conditions.
- Applying the patch is relatively simple.
- The patch can be removed to examine the tank wall.
- There is a high probability the system will work on active leak sites.

The following are disadvantages to the magnetic patch concept:

• The patch dimensions will limit the area that can be sealed. Patches placed next to each other may allow for larger areas to be sealed, but this needs to be tested.

MILESTONES

The TRRS vehicle work is funded by TTP SR10C131 and the Tank Remote Repair System task has two milestones in FY02. The first milestone is entitled, "Complete the Large Scale Vehicle Test Platform", or Tank Mock-up, and is milestone number 175-3.2-1. SRTC designed the large scale vehicle test platform to include a 5 inch diameter riser, several wall section of various thickness, a lower tank wall knuckle, a tank bottom section, and removable plates in the wall, knuckle, and bottom. SRTC hired a sub-contractor to fabricate and install it in SRS bldg. 723-A. Figures 11 and 12 show the Tank Mock-up layout and the completed large scale vehicle test platform.

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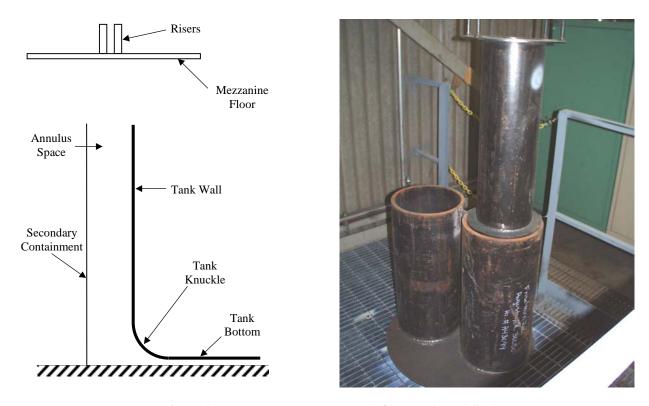


Figure 11 – Tank Mock-up: Layout (left) and Risers (right)



Figure 12 – Tank Mock-up: Upper Wall (left) and Lower Wall, Knuckle, and Tank Bottom (right)

The second milestone is entitled, "Issue TRRS Conceptual Design" and is milestone number 175-3.2-2. This report documents the TRRS conceptual design.

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CONCLUSION

This report discusses two TRRS concepts. The first concept uses a magnetic wheeled wall crawler to deliver an epoxy patch and the second concept uses a magnetic wheeled wall crawler to deliver a magnetic patch. The report includes advantages and disadvantages for each concept. The magnetic patch concept is the recommended due to the easier application in the tank annulus space, positive preliminary test results, and high probability of stopping active leak sites. The magnetic patch concept is being tested in the laboratory this fiscal year. If the test results are positive, the TRRS system should be thoroughly evaluated in a test environment and deployed as needed.

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- 4. Kriikku, E. M., Functions and Requirements for the Tank Remote Repair System (U). WSRC-TR-2001-00272, Savannah River Site, Aiken, SC 29808 (9/5/2001).
- 5. Subramanian, K. H., *Leak Mitigation System Materials Selection Program Plan*, WSRC-TR-2002-00066, Savannah River Site, Aiken, SC 29808 (2/2002).

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APPENDIX 1 - Type I Tank Details

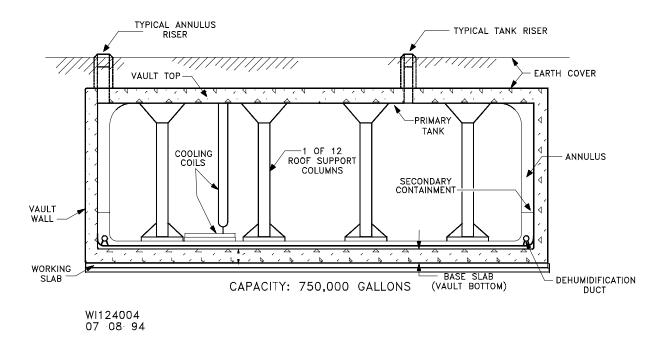


Figure 13 – Type I Tank

Waste Tank Capacity 750,000 gallons

Primary Tank Shell Closed top construction – 75 foot D x 24.5 foot H.

Constructed of carbon steel, ½ inch thick throughout

Design Temperature 220°F max Design Pressure 1.4 psi max

Cooling 36 parallel coils supported by the roof with 2 horizontal coils across the tank

bottom

Secondary Containment Steel pan – 80 foot D x 5 foot H. Constructed of carbon steel, ½ inch thick

throughout.

Roof Support Twelve 2 foot OD, ½ inch thick carbon steel columns filled with concrete.

Columns are supported by the tank bottom.

Concrete Vault 22-inch thick wall and roof. 30-inch thick floor. Waterproofed on outside of

wall, top of roof, and under foundation.

Radiation Shielding 9-foot thick layer of earth on top of roof.

Location Tanks 1 through 8 are in F Area and Tanks 9 through 12 are in H Area.

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APPENDIX 2 – Type II Tank Details

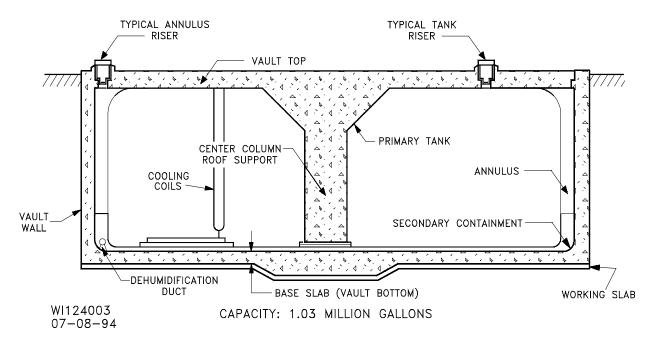


Figure 14 – Type II Tank

Waste Tank Capacity 1,030,000 gallons

Primary Tank Shell Closed top construction – 85 foot D x 27 foot H.

Constructed of carbon steel. Thicknesses: top/bottom $-\frac{1}{2}$ inch; upper knuckle

plate -9/16 inch; wall -5/8 inch; lower knuckle plate -7/8 inch.

Design Temperature 350°F max Design Pressure 2.0 psi max

Cooling 44 parallel coils supported by the roof and 4 horizontal coils across the bottom.

Secondary Containment Saucer Construction – 90 foot D x 5 foot H. Constructed of carbon steel, ½ inch

thick throughout.

Roof Support
Once central concrete column clad with ½ inch carbon steel.
Concrete Vault
33-inch thick wall, 45-inch thick roof, 42-inch thick floor.
Radiation Shielding
45-inch thick concrete roof with no earth overburden.

Location Tanks 13 through 16 are in H Area.

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APPENDIX 3 – Type III Tank Details

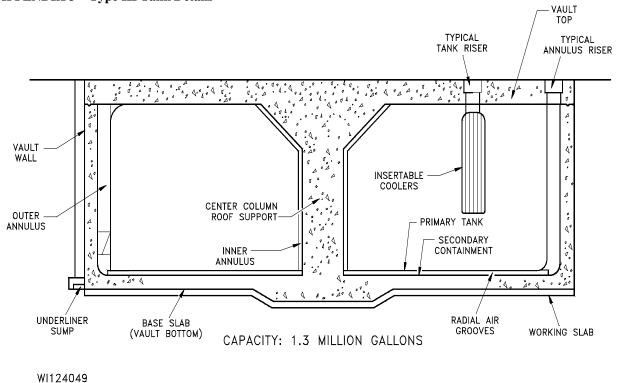


Figure 15 - Type III Tank

Waste Tank Capacity 1,300,000 gallons

07-11-94

Primary Tank Shell Closed top construction – 85 foot D x 33 foot H.

Constructed of carbon steel. Thicknesses: top/bottom – $\frac{1}{2}$ inch; upper knuckle plate – $\frac{3}{4}$ inch; outer wall tapers from $\frac{3}{4}$ inch at bottom to $\frac{1}{2}$ inch at top. Inner wall tapers from $\frac{5}{8}$ inch at bottom to $\frac{1}{2}$ inch at the top. Full stress relief is in

place at 1100°F.

Design Pressure 2.2 psi max

Cooling Type III tanks have cooling coil bundles. Bottom coiling for this type is

provided by forced air glow through grooved channels in the concrete beneath

the tank.

Secondary Containment Closed top construction – 90 foot D x 5 foot H. Constructed of carbon steel.

Roof Support
Once central concrete column supported on concrete foundation.
Concrete Vault
30-inch thick walls, 48-inch thick roof, 42-inch thick floor.
Radiation Shielding
48-inch thick concrete roof with no earth overburden.

Location Tanks 33 and 34 are in F Area. Tanks 29 through 32 are in H Area.

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APPENDIX 4 – Type IIIA Tank Details

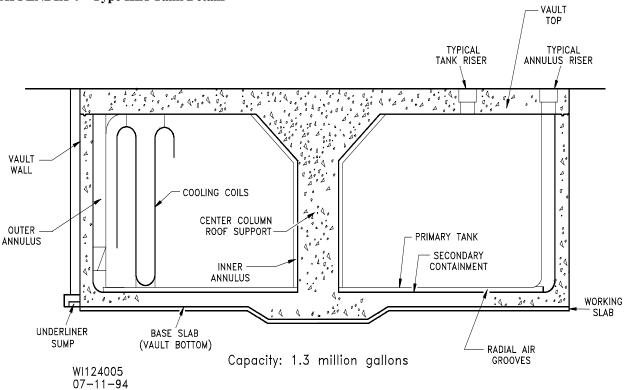


Figure 16 - Type IIIA Tank

Waste Tank Capacity 1,300,000 gallons

Primary Tank Shell Closed top construction – 85 foot D x 33 foot H.

Constructed of carbon steel. Thicknesses: top/bottom – $\frac{1}{2}$ inch; upper knuckle plate – $\frac{3}{4}$ inch; outer wall tapers from $\frac{3}{4}$ inch at bottom to $\frac{1}{2}$ inch at top. Inner wall tapers from $\frac{5}{8}$ inch at bottom to $\frac{1}{2}$ inch at the top. Full stress relief is in

place at 1100°F.

Design Pressure 2.2 psi max

Cooling Type III tanks have vertical cooling coils supported from the tank bottom.

Bottom coiling for this type is provided by forced air glow through grooved

channels in the concrete beneath the tank.

Secondary Containment Closed top construction – 90 foot D x 5 foot H. Constructed of carbon steel.

Roof Support Once central concrete column supported on concrete foundation. Annulus space

around column.

Concrete Vault 30-inch thick walls, 48-inch thick roof, 42-inch thick floor.

Radiation Shielding 48-inch thick concrete roof with no earth overburden.

Location Tanks 33 and 34 are in F Area. Tanks 29 through 32 are in H Area.

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